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SIMPLIFIED METHOD OF HEAT CALCULATIONS OF OIL-AIR HEAT EXCHANGERS

Notation:

- α – convection heat-transfer coefficient, $W/(m^2 \cdot K)$
- c – mean heat capacity, $kJ/(m^3 \cdot K)$
- d – diameter, m
- F – heating surface area, m^2
- k – over-all heat-transfer coefficient, $W/(m^2 \cdot K)$
- L – height of fin, m
- λ – thermal conductivity, $W/(m \cdot K)$
- m – parameter of fin, m
- M – mass rate of fluid flow, kg/s
- p – pitch of fins, m
- r – radius, m
- s – thickness of fin, m
- t – temperature, K
- ρ – density, kg/m^3
- μ – viscosity coefficient, $kg/(m \cdot s)$
- w – velocity, m/s
- V – volumetric rate of fluid flow, m^3/s
- Q – heat transfer rate, W
- η – efficiency

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1. INTRODUCTION

New constructions of heat exchangers require research on the intensification of heat transfer realized by Mean Direct Action on the Flow or Surface Development methods [1, 4, 5]. Intensification of heat transfer in exchanger increases over-all heat transfer coefficient and efficiency, also reduces construction materials costs. For calculation of heat exchangers designs Mean Temperature Difference method and Heat Effectives one are used [6, 8]. The both methods are based on universal equal of energy balance. The aim this paper is new method of calculations oil-air exchangers made of cross-finned aluminium pipes.

2. UNIVERSAL EQUATIONS OF HEAT TRANSFER

Heat transfer rate of oil-air exchangers is described by equations (1, 2):

$$Q = V_a c_a (t_a'' - t_a')$$
 (1)

where:

V_a – volumetric rate of air flow,

c_a – mean heat capacity of air,

t_a' – inlet air temperature,

t_a'' – outlet air temperature.

$$Q = kF (\bar{t}_f - \bar{t}_a)$$
 (2)

where:

k – over-all heat transfer coefficient,

F – heating surface area,

\bar{t}_f – mean temperature of oil,

\bar{t}_a – mean temperature of air.

Over-all heat transfer coefficient [1, 8] is:

$$k = \frac{1}{\frac{\varphi_o}{\alpha_f} + \frac{1}{\alpha_r}}$$
 (3)

where:

α_f – convection heat transfer coefficient from oil to wall,

α_r – reduced heat transfer coefficient,

φ_o – finning ratio.

$$\Phi_o = \frac{F}{F_r} \quad (4)$$

where:

F – surface finned area,

F_r – surface area of smooth pipe.

Influence of efficiency on heat transfer describes reduced heat-transfer coefficient by equation:

$$\alpha_r = \alpha_o \left(\frac{F_m}{F_r} + \frac{F_z}{F_r} \eta \right) \quad (5)$$

where:

α_o – convection heat-transfer coefficient of smooth element,

F_m – surface area between fins,

F_z – surface area of fins,

F_r – surface area of smooth pipe,

η – efficiency.

Figure 1 illustrates the cross-finned pipe with circular fins of constant thickness.

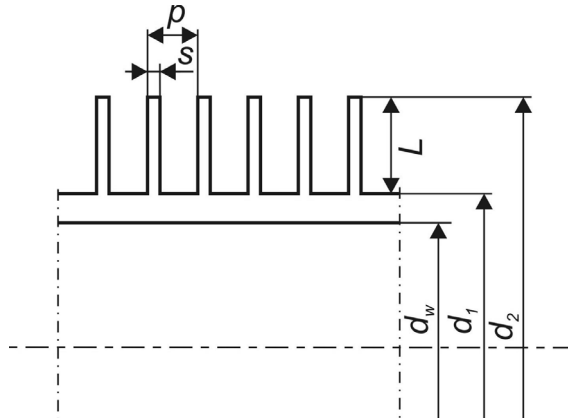


Fig. 1. The cross-finned pipe: d_w – inner diameter of pipe, d_1 – outer diameter of pipe, d_2 – outer diameter of finned pipe, L – height of fin, s – thickness of fin, p – pitch of fins

For diameters ratio of pipe $d_1/d_w < 2$ it is possible to calculate over-all heat-transfer coefficient as for plane wall [7], by equation (3).

3. RESEARCH OF ELEMENTS OF THE HEAT EXCHANGERS MADE OF CROSS-FINNED ALUMINIUM PIPES

The tested element of heat exchangers has the following geometric, flow, and temperature parameters:

– inner diameter of element	$d_w = 0.025 \text{ m}$,
– outer diameter of element	$d_1 = 0.030 \text{ m}$,
– outer diameter of finned element	$d_2 = 0.052 \text{ m}$,
– height of fin	$L = 0.011 \text{ m}$,
– thickness of fin	$s = 0.00045 \text{ m}$,
– pitch of fin	$p = 0.00252 \text{ m}$,
– inlet air temperature	$t'_a = 18.3 \text{ }^\circ\text{C}$,
– outlet air temperature	$t''_a = 23.5 \text{ }^\circ\text{C}$,
– inlet oil temperature	$t'_f = 70.1 \text{ }^\circ\text{C}$,
– outlet oil temperature	$t''_f = 66.6 \text{ }^\circ\text{C}$,
– mass rate of oil flow	$M_f = 0.35 \text{ kg/s}$,
– volumetric rate of air flow	$V_a = 0.365 \text{ m}^3/\text{s}$,
– surface area of air flow	$F_a = 0.00317 \text{ m}^2$,
– surface area of oil flow	$F_f = 0.0112 \text{ m}^2$,
– length of element	$l = 0.295 \text{ m}$,
– simplex of diameters	$d_1/d_2 = 1.2$,
– quantity of elements	$n = 23$,
– heat surface area of exchanger	$F = 1.15 \text{ m}^2$.

According to Schmidt [9] efficiency of circular fin is described by equation:

$$\eta = \frac{tgh(mL_c\varphi)}{mL_c\varphi} \quad (6)$$

where:

$$\varphi = 1 + 0.35 \ln \left(1 + \frac{L_c}{r_1} \right) = 1 + 0.35 \ln \left(1 + \frac{0.0114}{0.015} \right) = 1.198,$$

$$L_c = r_{2c} - r_1 = 0.0264 - 0.015 = 0.0114 \text{ m},$$

$$r_1 = \frac{d_1}{2} = \frac{0.030}{2} = 0.015 \text{ m},$$

$$r_2 = \frac{d_2}{2} = \frac{0.052}{2} = 0.026 \text{ m,}$$

$$r_{2c} = \frac{d_2 + s}{2} = \frac{0.052 + 0.00045}{2} = 0.0264 \text{ m.}$$

Parameter of fin is:

$$m = \sqrt{\frac{2\alpha}{\lambda s}} = \sqrt{\frac{2 \cdot 45.4}{165 \cdot 0.00045}} = 34.96 \text{ m,}$$

where:

convection of heat-transfer coefficient delivered to surface area of smooth pipe

$$\alpha_o = 45.4 \text{ W}/(\text{m}^2 \cdot \text{K}),$$

thermal conductivity of aluminium $\lambda = 165 \text{ W}/(\text{m} \cdot \text{K}),$

thickness of fin $s = 0.00045 \text{ m,}$

$$m \cdot L_c = 34.96 \cdot 0.0114 = 0.399 \text{ m}^2,$$

$$\eta = \frac{\text{tgh}(34.96 \cdot 0.0114 \cdot 1.198)}{34.96 \cdot 0.0114 \cdot 1.198} = 0.97.$$

According to Brandt [9] efficiency of circular fin is described by equation:

$$\eta = \frac{2r_1}{2r_1 + L_c} \frac{\text{tgh } mL_c}{mL_c} \left[1 + \frac{\text{tgh } mL_c}{2mr_1} + 0.071882 \frac{(\text{tgh } mL_c)^{3.7482}}{(mr_1)^{1.481}} \right] \quad (7)$$

where:

$$r_1 = 0.015 \text{ m, } L_c = 0.014 \text{ m, } m = 34.96 \text{ m.}$$

$$\eta = \frac{2 \cdot 0.015}{2 \cdot 0.015 + 0.014} \frac{\text{tgh } 34.96 \cdot 0.014}{34.96 \cdot 0.014} \left[1 + \frac{\text{tgh}(34.96 \cdot 0.014)}{2 \cdot 34.96 \cdot 0.015} + 0.071882 \frac{(\text{tgh } 34.96 \cdot 0.014)^{3.7482}}{(34.96 \cdot 0.014)^{1.481}} \right] = 0.93.$$

Efficiency of circular fin is described [9] also by equation:

$$\eta = \frac{1}{1 + \frac{1}{3}(mL_c)^2 \sqrt{\frac{r_{2c}}{r_1}}} \quad (8)$$

where:

$$mL_c = 0.399 \text{ m}^2, r_{2c} = 0.0264 \text{ m}, r_1 = 0.015 \text{ m}.$$

$$\eta = \frac{1}{1 + \frac{1}{3}(0.399)^2 \sqrt{\frac{0.0264}{0.015}}} = 0.93.$$

4. RESEARCH OF HEAT TRANSFER COEFFICIENTS

Heat transfer coefficient on oil side

Surface area of oil flow is:

$$F_f = 23 \frac{\pi d_w^2}{4} = 23 \frac{\pi \cdot 0.025^2}{4} = 0.0112 \text{ m}^2.$$

Velocity of oil is:

$$w_f = \frac{M_f}{\rho F_f} = \frac{0.35}{864 \cdot 0.0112} = 0.036 \text{ m/s},$$

where: density of oil $\rho_f = 864 \text{ kg/m}^3$.

Reynolds number is:

$$\text{Re} = \frac{w_f d_w \rho_f}{\mu} = \frac{0.036 \cdot 0.025 \cdot 864}{60.558 \cdot 10^{-4}} = 128.4,$$

where:

$$\text{mean temperature of oil } \bar{t}_f = \frac{70.1 + 66.6}{2} = 68.4 \text{ }^\circ\text{C},$$

dynamic viscosity coefficient of oil [10] $\mu = 60.558 \cdot 10^{-4} \text{ kg/(m}\cdot\text{s)}$.

According to Mikheyev [7] for laminar flow of oil heat transfer coefficient is described by similarity equation:

$$\text{Nu} = 1.4 \text{Re}^{0.4} \text{Pr}^{0.33} \left(\frac{d}{l} \right)^{0.4} \quad (9)$$

Prandtl number is:

$$\text{Pr} = \frac{c_f \mu}{\lambda_f} = \frac{2.137 \cdot 60.558 \cdot 10^{-4}}{0.121} = 107.0,$$

where:

thermal conductivity of oil [10] $\lambda_f = 0.121 \text{ W/(m}\cdot\text{K)}$,

mean heat capacity of oil [10] $c_f = 2.137 \text{ kJ/(kg}\cdot\text{K)}$.

Nusselt number is:

$$\text{Nu} = \frac{\alpha_f d_w}{\lambda} = \frac{\alpha_f 0.025}{0.121} = 1.4 \cdot 128.4^{0.4} \cdot 107^{0.33} \left(\frac{0.025}{0.295} \right)^{0.4},$$

hence heat-transfer coefficient

$$\alpha_f = 82.0 \text{ W/(m}^2\cdot\text{K)}.$$

Heat-transfer coefficient on air side

Velocity of air is:

$$w_a = \frac{V_a}{F_a} = \frac{0.365}{0.00317} = 11.5 \text{ m/s},$$

According to Schack [3] convective heat-transfer coefficient for smooth element is:

$$\alpha_o = (3.5 + 0.00185 \bar{t}_a) \frac{w_a^{0.8}}{d_2^{0.2}} = (3.5 + 0.00185 \cdot 20.9) \frac{11.5^{0.8}}{0.052^{0.2}} = 45.4 \text{ W/(m}^2 \cdot \text{K)},$$

where:

outer diameter $d_2 = 0.052 \text{ m}$,

mean temperature of air $\bar{t}_a = \frac{18.3 + 23.5}{2} = 20.9 \text{ }^\circ\text{C}$.

The surface area of fin is:

$$F_z = 2\pi(r_2^2 - r_1^2) = 2\pi(0.026^2 - 0.015^2) = 0.00283 \text{ m}^2.$$

The surface area of smooth pipe on one pitch is:

$$F_r = 2\pi r_1 p = 2\pi \cdot 0.015 \cdot 0.00254 = 0.000239 \text{ m}^2.$$

The inner surface area of pipe is:

$$F_w = 2\pi r_w p = 2\pi \cdot 0.012 \cdot 0.00254 = 0.00191 \text{ m}^2.$$

The surface area between fins on one pitch is:

$$F_m = F_r - \pi d_1 s = 0.000239 - \pi \cdot 0.030 \cdot 0.00045 = 0.000197 \text{ m}^2.$$

The reduced convection heat-transfer coefficient is:

$$\alpha_r = \alpha \left(\frac{F_m}{F_r} + \frac{F_z}{F_r} \eta \right) = 45.4 \left(\frac{0.000197}{0.000239} + \frac{0.00283}{0.000239} \cdot 0.95 \right) = 548.1 \text{ W}/(\text{m}^2 \cdot \text{K}).$$

The over-all heat transfer coefficient calculated by equations (3) and (4) is:

$$k = \frac{1}{\frac{\varphi_o}{\alpha_f} + \frac{1}{\alpha_r}} = \frac{1}{\frac{1.8}{82} + \frac{1}{548.1}} = 42.0 \text{ W}/(\text{m}^2 \cdot \text{K}).$$

where:

$$\varphi_o = \frac{F}{23 \cdot \pi d_1 \cdot l} = \frac{.15}{23 \cdot \pi \cdot 0.03 \cdot 0.295} = 1.8.$$

The heat-transfer ratio of heat exchanger is:

$$Q = V_a \cdot c_a (t_a'' - t_a') = 0.365 \cdot 1.28 (23.5 - 18.1) = 2.43 \text{ kW}.$$

The mean temperature difference is:

$$\Delta t_m = \bar{t}_f - \bar{t}_p = 68.4 - 20.9 = 47.5 \text{ }^\circ\text{C}.$$

The over-all heat-transfer coefficient calculated by equation (2) is:

$$k = \frac{Q}{F \Delta t_m} = \frac{2340}{1.15 \cdot 47.5} = 45.0 \text{ W}/(\text{m}^2 \cdot \text{K}).$$

The calculation error of over-all heat-transfer coefficient is:

$$\Delta = \frac{45 - 42}{45} \cdot 100\% = 6.7\%.$$

5. INFERENCES

- Model researches carried out on an experimental post and heat calculations make possible the identification of over-all heat-transfer coefficient in oil-air heat exchanger made of aluminium cross-finned pipes with circular fins.
- Difference of the value of over-all heat transfer coefficient calculated by simplified method and Mean Temperature Difference one comes to 6.7%.
- Influence efficiency of fin on heat transfer is described by the reduced heat transfer coefficient.
- The maximal difference between efficiency of fin calculated by three methods comes to 4.0%.
- Elaborated simplified method makes possible the identification of construction parameters and designed oil-air heat exchangers.

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REFERENCES

- [1] *Karczewski K.*: Wpływ mikrouzębrowania powierzchni równoległoprądowych rekuperatorów metalowych na ich cechy konstrukcyjne i eksploatacyjne, UWN-D AGH, Kraków, 2000
- [2] *Karczewski K.*: Metallurgy and Foundry Engineering, 29 (2003), 97–107
- [3] *Karczewski K.*: Obliczenia cieplne rekuperatorów metalowych dla pieców przemysłowych, UWND AGH, Kraków, 2004, SU 1667
- [4] *Karczewski K.*: Metallurgy and Foundry Engineering, 33 (2007), 129–139
- [5] *Karczewski K.*: Metallurgy and Foundry Engineering, 34 (2008), 39–50
- [6] *Karczewski K.*: Metallurgy and Foundry Engineering, 36 (2010), 37–46
- [7] *Mikheyev M.*: Fundamentals of Heat Transfer, Mir Publishers, Moscow 1968
- [8] *Senkara T.*: Obliczenia pieców grzewczych w hutnictwie żelaza, Wydawnictwo Śląsk, Katowice, 1983
- [9] *Taler J., Duda P.*: Rozwiązywanie prostych i odwrotnych zagadnień przewodzenia ciepła, WNT, Warszawa 2003
- [10] *Razniewicz K.*: Tablice cieplne z wykresami, WNT, Warszawa 1966, Wyd. 1